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propagating signals are usually allocated at different wavelengths. Thus, we can suppress the reflected light by using optical filters at the receiver. However, we cannot remove the multiple reflected lights in such a way and the multiple reflected lights causes a relative intensity noise. The magnitude of the relative intensity noise is proportional to the square of optical amplifier gain. Thus the relative intensity noise limits the maximum available amplifier gains of the bidirectional transmission systems and networks.

Figure 1 shows a schematic diagram of a conventional wavelength-division multiplexing (WDM) bidirectional transmission system. It also illustrates a relative intensity noise generation path in the bidirectional transmission system. Each node comprises a transmitter (TX) that generates the WDM signal to be transmitted to the other node and a receiver (RX) that receiving the WDM signals transmitted from said the other node. Also an optical circulator (Cir) will be installed at each node to route the receiving and the transmitting signals. Several bidirectional optical amplifiers (BA) are installed in the bidirectional transmission link deployed between two nodes to compensate for the loss of optical fibers (10).

In this WDM bidirectional transmission system,

the output wavelengths of the two nodes are different. We can allocate the wavelengths of the counter-propagating signals according to two different methods: band split scheme and wavelength-interleaved scheme. In the band split bidirectional transmission system as shown in Figure 2, the wavelengths of WDM signals being transmitted in the same direction are contiguous, while the wavelengths of counter-propagating signals are allocated in different wavelength bands. In the wavelength-interleaved bidirectional transmission systems as shown in Figure 3, the counter-propagating signals are interlaid in wavelength domain.

By allocating the different wavelengths for the optical signals propagating in the opposite directions, we can eliminate the reflected noisy light generated by the simple reflection. In other words, even if the signal propagating in one direction is reflected at the optical fibers (10) or other optical components and then combines with the other direction signal, the reflected light will be eliminated at the receiver (RX) by an optical filter. However, the optical filter installed at the receiver (RX) cannot remove the multiple reflected noisy lights because their wavelengths are same as those of the signal lights.

For an example, a signal reflected at an optical fiber (10) would be amplified at the optical amplifier (BA). If this reflected signal were to be reflected again at another optical fiber, it would be amplified again, and combined with the original signal as shown in Figure 1. In such a case, the wavelength of the multiple-reflected noisy signal is identical to that of the original signal, and thus would not be removed by the optical filter installed at the receiver (RX). Therefore it is necessary a method to suppress the multiple-reflected light in a bidirectional optical transmission system.

In occasion, it is necessary to receive or transmit selected signals at an intermediate node of the bidirectional transmission link. In such a case the bidirectional WDM transmission systems further comprises add/drop multiplexer (ADM) at the intermediate node. Figure 4 is a schematic diagram of a WDM bidirectional transmission system further comprising a conventional add/drop multiplexer (ADM) that add/drop signals with specific wavelengths.

The conventional add/drop multiplexer (ADM) comprises a de-multiplexer (D), 2 x 2 optical switches (Sw) and a multiplexer (M).

In this case, two optical circulators (Cir) are

used to separate/combine the counter propagating at  
the input and the output port of the add/drop  
multiplexer (ADM). The optical signals transmitted  
from left to right is first routed to the de-  
multiplexer by the optical circulator (Cir) and then  
separated as their wavelengths by the de-multiplexer  
(D). The 2 x 2 optical switches (Sw) connected to the  
output ports of the de-multiplexer establish  
transmission paths for the demultiplexed signals to be  
dropped or passed though the add/drop multiplexer  
(ADM). We can add the same wavelength signals with the  
dropped signals though the optical switch. The outputs  
of the optical switches are multiplexed by the  
multiplexer (M) and enter into another optical  
circulator. The optical circulator route the signals  
into the optical fiber.

Here, the relative intensity noise can be  
generated through the transmission path of the signal  
passing through the ADM as shown in Figure 4.

Therefore, a means for suppressing the relative  
intensity noise should be incorporated with the with  
the ADM.

#### SUMMARY OF THE INVENTION

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The present invention is contrived in order to solve the above problems. It is an object of the present invention to provide a 4-port wavelength selective router that effectively routes the counter-propagating signals over a single optical fiber while suppressing the relative intensity noise induced by the multiple back reflections. The 4-port wavelength selective router in accordance with the present invention has four ports (1, 2, 3, 4) and three internal signal transmission paths between port pairs ((1,2), (2,3), (3,4)). The 4-port wavelength selective router routes two groups (Group A and Group B) of signals propagating counter-directionally. The wavelengths of the signals included in Group A are different from those of the signals included in Group B. When the Group A signals enter at port (2) and output through port (3), and Group B signals enter at port (3) and output through port (2), the signal transmission characteristics of the router is characterized as follows; between port (2) and (3) only the Group A signals can be transmitted from port (2) to port (3), and no signal can be transmitted oppositely; between port (1) and (2), and port (3) and (4) only the Group B signals or both Group A and B

signals can be transmitted, but both Group A and B signals are not transmitted simultaneously (in other words, between ports (1) and (2), and ports (3) and (4) at least one port pairs can transmit only the Group B signals); between port (1) and (2), and port (3) and (4) optical signals can be transmitted bidirectionally, but at least one port pair can transmit the signals from port (1) to (2) or from port (3) to (4); and signals inputted to a specific port (1, 2, 3, 4) can be transmitted to only one port (1, 2, 3, 4).

#### BRIEF DESCRIPTION OF THE DRAWINGS

Exemplary embodiments of the present invention will be described in conjunction with the drawings in which:

Figure 1 shows a schematic diagram for the conventional WDM bidirectional transmission system;

Figure 2 and Figure 3 show the wavelength allocation methods in WDM bidirectional transmission systems and networks;

Figure 4 shows a schematic diagram of bidirectional transmission system comprising a conventional add/drop multiplexer (ADM);

Figure 5 shows a schematic diagram of the 4-port wavelength selective router according to the present invention;

Figure 6 illustrates the suppression of the multiple reflections with the router in Figure 5;

Figure 7 shows a schematic diagram for the 4-port wavelength selective router according to the first embodiment of the present invention;

Figure 8, Figure 9 and Figure 10 show the propagation path and the polarization state of the optical wave inputted at the port (1) of the router in Figure 7;

Figure 11, Figure 12 and Figure 13 show the propagation path and the polarization state of the optical wave inputted through port (2) of the router in Figure 7;

Figure 14 shows the propagation path of the optical wave inputted at port (3) of the router in Figure 7;

Figure 15 shows the propagation path of the optical wave inputted at port (4) of the router in Figure 7;

Figure 16 and Figure 17 show the propagation path and the polarization state of the optical wave that is reflected at the wavelength selective filter (WF);



Figure 18 shows the transmission characteristics of the wavelength selective filter (WF) of Figure 7 according to an embodiment of the present invention;

Figure 19 shows the transmission characteristics of the wavelength selective filter (WF) of Figure 7 according to another embodiment of the present invention;

Figure 20 shows a schematic diagram of the 4-port wavelength selective router according to another embodiment of the present invention;

Figure 21 and 22 show the transmission characteristics of wavelength-selective coupler in the router in Figure 20;

Figure 23, 24, 25, and 26 show schematic diagrams of the 4-port wavelength selective router according to other embodiments of the present invention;

Figure 27 shows a schematic diagram of the bidirectional add/drop multiplexer (ADM) using the router of the present invention.

<Explanations for main symbols in the drawings>

4pr: 4-port optical path router, 10: optical fiber,

12: thin film, 14: anti reflection (AR) coating,

16a, 16b: dielectric coating,

BA: bidirectional optical amplifier,  
 BC1,BC2,BC3,BC4: polarization splitter,  
 Cir,Cir1: optical circulator,      D: de-multiplexer,  
 Fil1,Fil2: optical filter,  
 5    FR1,FR2: non-reciprocal rotator, M: multiplexer,  
 Re: receiving terminal,  
 RR1,RR2: reciprocal rotator,      RX: receiver,  
 Sw: optical switch,      TX: transmitter,  
 Tr: transmitting terminal,  
 WF: wavelength selective filter,  
 WF1,WF2,WF3: wavelength filter,  
 WSC,WSC1: wavelength selective coupler,  
 Isol,Iso2: optical isolator,

#### 5    DETAILED DESCRIPTION OF THE EMBODIMENTS

The 4-port wavelength selective router (4pr) in  
 accordance with the present invention is used in order  
 to effectively route two groups of counter-propagating  
 20    signals over a single optical fiber and also to  
 suppress the relative intensity noise induced by  
 multiple back reflections. The above two groups are  
 defined as follows: the first group (Group A) consists  
 of one or more optical signals of different  
 25    wavelengths. The second group (Group B) consists of

one or more optical signals of different wavelengths  
excluding the signals included in Group A. Here the  
methods for dividing the optical signals (Group A,  
Group B) are above mentioned band split scheme or  
wavelength-interleaved scheme.

As shown in Figure 5, the 4-port wavelength  
selective router (4pr) has 4 ports (1, 2, 3, 4). Thus  
the possible combinations of port pairs are 6 in total  
((1,2), (2,3), (3,4), (1,3), (2,4), (1,4)). The  
internal signals transmission paths exist between port  
pairs (1) and (2), ports (2) and (3), and ports (3)  
and (4). Whereas there is no signal transmission path  
between ports (1) and (3), ports (2) and (4), and  
ports (1) and (4).

At port (2) Group A signals are inputted and  
Group B signals are outputted. At port (3) Group B  
signals are inputted and Group A signals are outputted.

The signals transmission characteristics of the  
ports pairs in the 4-port wavelength selective router  
(4pr) in accordance with the present invention satisfy  
the following rules. First, between port (2) and (3),  
only the Group A signals can be transmitted from port  
(2) to port (3). No signals can be transmitted in the  
opposite direction. Second, between ports (1) and (2),  
and ports (3) and (4) the Group B signals or both

Groups A and B signals are transmitted, but both Group A and B signals are not transmitted simultaneously between ports (1) and (2), and ports (3) and (4). In other words, between the two port pairs ((1,2), (3,4)) at least one port pair should transmit only Group B signals. Third, between ports (1) and (2), and ports (3) and (4) optical waves are transmitted bidirectionally but at least one port pair should transmit signals only one direction. Namely, between the two port pairs, at least one port pair should transmit signal from port (1) to (2) or port (3) to (4). Fourth, signals inputted to a specific port (1, 2, 3, 4) cannot be transmitted to more than one port (1, 2, 3, 4) simultaneously.

The number of 4-port wavelength selective router (4pr) modules satisfying the above mentioned rules is eight in total. Table 1 shows the 4-port wavelength selective router (4pr) module types and the optical signal transmission characteristics of the ports pairs. Here X denotes that no optical wave can pass between the two ports.

# 【Table 1】

The configurable 4-port wavelength selective

router (4pr) modules and signal transmission characteristics of them.

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5           Examining module #1 of Table 1, the Group B signal can be transmitted from port (1) to port (2), only the Group A signal from port (2) to port (3), and only the Group B signal from port (3) to port (4). Between all other ports and in the other direction, signals are not transmitted. Continuing to examine module #8 in Table 1, only Group B signal can be transmitted from port (1) to port (2) and only the Group A signal from port (2) to port (3). Between ports (3) and (4), both Groups A and B signals are transmitted bidirectionally. And no optical waves are transmitted in other ports pairs and in the other direction.

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20           As shown in Figure 6, the 4-port wavelength selective router (4pr) can suppress the multiple reflections generated in the bidirectional transmission systems and networks. When ports (1) and (4) are connected and the counter-propagating signals were inputted/outputted through the ports (2) and (3),  
25           the signals being inputted at the port (2) cannot be

transmitted from port (3) to port (2) and vice versa.  
The signals being inputted at the port (3) cannot be  
transmitted from port (3) to port (1) and vice versa.

5        Figure 7 shows the 4-port wavelength selective  
router (4pr) according to an embodiment of the present  
invention. The router (4pr) comprises polarization  
splitters (BC1, BC2, BC3, BC4), reciprocal  
polarization rotators (RR1, RR2), Faraday non-  
reciprocal polarization rotators (FR1, FR2), and  
wavelength selective filter (WF).

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5        The polarization splitters (BC1, BC4) separates  
an optical wave with an arbitrary polarization, which  
is inputted through each port (1, 2, 3, 4), into two  
optical waves that are polarized perpendicular with  
respect to the z-axis (Parallel to the x or y-axis).  
The above polarization splitters also combine two  
optical polarized perpendicularly with respect to the  
z-axis. The polarization splitters (BC2, BC3) cause a  
displacement in the x-axis. Namely, extraordinary wave  
20        having a polarization in x-axis direction is refracted  
in x-axis direction at the polarization splitters (BC2,  
BC3). While ordinary waves having a polarization in y-  
axis direction pass through the polarization splitters  
25        (BC2, BC3) without any refraction.

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5 The reciprocal polarization rotators (RR1, RR2) are composed of two rotators having opposite rotation directions (PAR; Positive Angle Rotator, NAR; Negative Angle Rotator). The two reciprocal polarization rotators (RR1, RR2) have opposite rotation directions. The combination of the reciprocal polarization rotators (RR1, RR2) and the non-reciprocal polarization rotators (FR1, FR2) is a means for the polarization rotation which makes either two orthogonal optical waves have parallel polarization or optical waves polarized in parallel have orthogonal polarizations.

5 The wavelength selective filter (WF) is a combination of three filters (WF1, WF2, WF3). The uppermost of these filters (WF1) in the x-direction, selects the signals passing from port (1) to (2). The filter located in the middle (WF2) selects the signals passing from ports (2) to (3), and the filter located on the bottom (WF3) will likewise the signals passing  
20 from ports (3) to (4).

25 Figure 8, Figure 9 and Figure 10 show the propagation path and the polarization state of the optical wave inputted at port (1) observed in x, y, and z directions, respectively. Here the optical wave

with an arbitrary polarization would be separated into ordinary and extraordinary waves on the y-z plane by the polarization splitter (BC1). The two orthogonal optical waves will be rotated  $+45^\circ$  and  $-45^\circ$ , respectively, by the reciprocal polarization rotator (RR1) and thus they will be polarized in parallel. The above two optical waves will be rotated in the same direction by the non-reciprocal polarization rotator (FR1), so that the polarization becomes parallel to the y-axis, and then pass through the second polarization splitter (BC2) without any displacement in x-direction. Therefore, the optical waves pass through the filter (WF1) located between the two polarization splitters (BC1, BC2). The optical waves then pass through the polarization splitter (BC3) as ordinary waves, and afterwards pass through the reciprocal polarization rotator (RR2) and the non-reciprocal polarization rotator (FR2). Here the polarizations of the two optical waves become orthogonal each other. Thus, the two optical waves are combined at the fourth polarization splitter (BC4) and then transmitted to port (2).

Following the identical principle, Figure 11, Figure 12 and Figure 13 show the propagation path and



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polarization state of an optical wave inputted at port (2) observed from the x, y, and z direction, respectively. Similarly with the case of the optical wave inputted at port (1), the optical wave is separated into two orthogonal optical waves. They pass through the fourth polarization splitter (BC4), the non-reciprocal polarization rotator (FR2), and the reciprocal polarization rotator (RR2). The polarizations of the optical waves become parallel to the x-axis after passing through the reciprocal polarization rotator (RR2). They pass through the third polarization splitter (BC3) as extraordinary waves and will be refracted into the -x-direction. Therefore they pass the filter (WF2) and will be refracted at the second polarization splitter (BC2) in -x-direction. They will then have orthogonal polarizations each other after passing the non-reciprocal polarization rotator (FR1) and the reciprocal polarization rotator (RR1). Finally the optical waves will be combined at the first polarization splitter (BC1) and be transmitted to port (3).

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The optical wave inputted at port (3) propagates with the same polarization state in the y-z plane as the optical wave inputted at port (1). However, as

illustrated in Figure 14, it passes the filter (WF3) and is transmitted to port (4).

The optical wave inputted at port (4) propagates with the same polarization state in the y-z plane as the optical wave input at port (2) up to the third polarization splitter (BC3). However, as illustrated in Figure 15, it is refracted at the third polarization splitter (BC3) in -x-direction and cannot be transmitted to any of the other ports (1, 2, 3).

In the above embodiments, the wavelength selective filter (WF) which is composed of the three filters (WF1, WF2, WF3) has the role of selecting the wavelength of the optical wave which will be transferred between the ports (1, 2, 3, 4). Each of the filters (WF1, WF2, WF3) passes the optical waves with specific wavelengths, but reflects or attenuates the optical waves with other wavelengths.

Figure 16 and Figure 17 show the propagation path and the polarization state of the optical waves inputted at ports (1) and (2), respectively and the propagation path and the polarization state of the optical waves reflected at the wavelength selective filter (WF).

The optical wave inputted at port (1) propagates

according to the same transmission paths in Figure 8  
up to wavelength selective filter (WF). After  
reflected at the filter (WF1) it passes the second  
polarization splitter (BC2) with the identical  
polarization state as the incident light. But as it  
passes the non-reciprocal polarization rotator (FR1)  
and the reciprocal polarization rotator (RR1), the  
polarization state becomes different by  $90^\circ$  with the  
incident light and then is inputted into the first  
polarization splitter (BC1). And as shown in Figure 16  
the reflected light does not transmitted into the port  
(1) or (3).

The optical wave inputted at port (2) propagates  
according to the same transmission paths in Figure 8  
up to wavelength selective filter (WF). After  
reflected at the filter (WF1) it passes the second  
polarization splitter (BC3) with the identical  
polarization state as the incident light. But as it  
passes the reciprocal polarization rotator (RR2) and  
the non-reciprocal polarization rotator (FR1), the  
polarization state becomes different by  $90^\circ$  with the  
inputted optical wave and then is inputted into the  
fourth polarization splitter (BC4). And as shown in  
Figure 17 the reflected light is does not transmitted  
into the port (2) or (4).



filter (WF1) and the filter (WF3) have the identical transmission characteristics and have periodic pass/stop-band. The filter (WF2) also has periodic pass/stop-band and its period is the identical to those of the above filter (WF1, WF3), but the pass-band is shifted by the half of the period from those of the above filters (WF1, WF3).

The signal transmission characteristics of a 4-port wavelength selective router (4pr) implemented by using the wavelength selective filter described in Figure 18 is equivalent to the module #1 of Table 1. Here by changing the wavelength selective filter, we can implement other modules. For example, if filter (WF1) is not used so that all optical waves can be transmitted from port (1) to port (2), and the signal transmission characteristics would be identical to the module #4 of Table 1. Similarly if the filter (WF3) is not used, the signal transmission characteristics would be equivalent to the module #6 of Table 1.

The wavelength selective filter in Figure 18 is suitable for the wavelength-interleaved bidirectional transmission systems and networks. We can implement 4-port wavelength selective router (4pr) to be used in band split bidirectional transmission systems and networks by changing the wavelength selective filter

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5 (WF) as shown in Figure 19. The wavelength selective filter (WF) can be implement by using a thin film (12) and dielectric coating techniques. One side of the thin film (12) has an anti-reflection (AR) coating (14) while the other side has dielectric coatings (16a, 16b, 16a). The above dielectric coating (16a, 16b, 16a) reflects the signals with specific wavelengths. The filter (WF1) and the filter (WF3) have the identical reflection bands. The dielectric coatings (16b) should provides a reflection bands so that the reflection bands of the filter (WF2) should not overlap with those of the filter (WF1) and the filter (WF3).

20 The optical path router (4pr) according to the present invention can also be implemented by combining conventional devices. Figure 20 illustrates an embodiment of the router comprising an optical circulator (Cir) and a wavelength selective coupler (WSC). The optical circulator (Cir) has an input port (a), an output port (c) and a common port (b), and the wavelength selective coupler (WSC) has two input/output ports (d, f) and a common port (e).

25 The connections are as follow: The input port (a) of the optical circulator (Cir) is connected to port

(1) and the common port (b) is connected to port (2). The output port (c) of the circulator (Cir) is connected to one of the input/output port (d) of the wavelength selective coupler (WSC), and the common input/output (e) of the wavelength selective coupler (WSC) is connected to port (3). The other input/output port (f) of the wavelength selective coupler (WSC) is connected to port (4). In this embodiment the signal transmission characteristics of the router (4pr) is equivalent to module #5 of Table 1.

The wavelength selective coupler (WSC) can be divided in to two different types; a wavelength-division multiplexer and a wavelength-interleaver. Figure 21 illustrates the signal transmission characteristics of the wavelength-division multiplexer . Between the common port (e) and the input/output port (d), signals within specific wavelength band can be transmitted bidirectionally, while between the common port (e) and the other input/output port (f), the signals within the other wavelength band excluding the previous one can be transmitted bidirectionally.

As shown in Figure 22, the signal transmission characteristics of the wavelength-interleaver are as

follows. The pass-band between the common port (e) and one of the input/output port (d) repeats with a specific period. Between the common port (e) and the other input/output port (f), the pass-band period is same but it is shifted by an half of the period from that of the common port (e) and the input/output port (d) pair.

The 4-port wavelength selective router (4pr) shown in Figure 23 replaces the optical circulator (Cir) of Figure 20 with a wavelength selective coupler (WSC1) and two optical isolators (Iso1, Iso2). The router (4pr) illustrated in Figure 23 is composed of two wavelength selective couplers (WSC, WSC1) and two optical isolators (Iso1, Iso2). Each wavelength selective coupler (WSC, WSC1) has two input/output ports ((d, f), (d', f')) and a common port (e, e') and each optical isolator (Iso1, Iso2) has one input (g, g') and one output (h, h') ports.

The connections are as follow: The input port (g') of the optical isolator (Iso2) is connected to port (1), and the output port (h') of the isolator is connected to one of the input/output port (f') of the wavelength selective coupler (WSC1). The common port (e') of the wavelength selective coupler (WSC1) is



connected to port (2) and the other input/output port  
(d') is connected to the other optical isolator's  
(Iso1) input port (g). This isolator's output port  
(h) is connected to one of the input/output ports (d)  
5 of the other wavelength selective coupler (WSC). The  
common port (e) of the wavelength selective coupler  
(WSC) is connected to port (3) and the other  
input/output port (f) of the wavelength selective  
coupler (WSC) is connected to port (4). In this  
embodiment the signal transmission characteristics of  
the router (4pr) is equivalent to module #3 of Table 1.

Figure 24 shows a schematic diagram for the 4-  
port wavelength selective router (4pr) according to  
another embodiment of the present invention: The  
second optical isolator (Iso2) of Figure 23 is  
inserted between one of the input/output ports (f) of  
the wavelength selective coupler (WSC) and port (4)

The optical path router (4pr) is composed of two  
20 wavelength selective coupler (WSC, WSC1) having two  
input/output ports ((d, f), (d', f')) and a common  
port (e, e'), and two optical isolator (Iso1, Iso2)  
having one input (g, g') and one output port (h, h').  
One of the input/output port (f') of the (WSC1) is  
25 connected to port (1) and the common port (e') is

connected to port (2). The other input/output port (d') of the wavelength selective coupler (WSC1) is connected to input port (g) of the optical isolator (Iso1) and output port (h) of the isolator (Iso1) is connected to one of input/output port (d) of the wavelength selective coupler (WSC). The common port (e) of the wavelength selective coupler (WSC) is connected to port (3) and the other input/output port (f) of the wavelength selective coupler (WSC) is connected to input port (g') of the isolator (Iso2). The output port (h') of the isolator (Iso2) is connected to port (4). In this embodiment the signal transmission characteristics of the router is equivalent to module #2 of Table 1.

Figure 25 shows a schematic diagram for the 4-port wavelength selective router (4pr) according to another embodiment of the present invention: Two optical isolators (Iso1, Iso2) and the wavelength selective coupler (WSC) of Figure 24 are replaced by an optical circulator (Cir1).

The router (4pr) is composed of a wavelength selective coupler (WSC1) having two input/output ports (d', f') and a common port (e') and an optical circulator (Cir1) with an input (a'), an output (c'), and a common port (b'). One of the input/output ports

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(f') of the wavelength selective coupler (WSC1) is connected to port (1) and the common port (e') is connected to port (2). The other input/output port (d') of the wavelength selective coupler (WSC1) is connected to the input port (a') of the optical circulator (Cir1) and the common port (b') of the circulator (Cir1) is connected to port (3). The output port (c') of the optical circulator (Cir1) is connected to port (4). In this embodiment the signal transmission characteristics of the router is equivalent to module #7 of Table 1.

The wavelength selective coupler (WSC, WSC1) of Figure 23, Figure 24, and Figure 25 is either a wavelength-division multiplexer or a wavelength-interleaver like the wavelength selective coupler (WSC) of Figure 20.

20 The wavelength selective router (4pr) shown in Figure 26 replaces the wavelength selective coupler (WSC) of Figure 20 with an optical circulator (Cir1) and two optical filters (Fil1, Fil2). The router (4pr) illustrated in Figure 26 is composed of two optical circulators (Cir, Cir1) and two optical filters (Fil1, Fil2). Each optical circulator has an input port (a, a'), an output port (c, c') and a common port (b, b'),

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and each optical filter (Fil1, Fil2) has different pass/stop-bands with one input (j, j') and one output (k, k') ports.

5 The connections are as follow: The input port (a) of the optical circulator (Cir) is connected to port (1), and the input/output port (b) of the circulator (Cir) is connected to port (2). The output port (c) of the circulator (Cir) is connected to the input port (j) of the optical filter (Fil1) and the other port (k) of the filter (Fil1) is connected to the input port (a') of the other circulator (Cir1). This circulator's input/output port (b') is connected to port (3). The output port (c') of the circulator (Cir1) is connected to the input port (j') of the optical filter (Fil2) and the output port (k') of the filter (Fil2) is connected to port (4). In this embodiment the signal transmission characteristics of the router is equivalent to module #4 of Table 1.

20 The optical filter (Fil1, Fil2) is a band pass filter which passes optical signals within a specific wavelength band while cutting off optical signals outside the band, or a comb filter having the repeated pass/stop. And it has the same signal transmission  
25 characteristics shown in Figure 21 or in Figure 22.

The pass and stop-bands of one optical filter (Fil1) are opposite to those of the other filter (Fil2).

Figure 27 illustrates the construction of a  
5 bidirectional add/drop multiplexer (ADM) using the  
wavelength selective router (4pr) according to the  
present invention. By connecting the conventional  
add/drop module used in unidirectional optical  
transmissions to port (4) and (1) of the optical  
router (4pr), one can implement a bidirectional  
add/drop multiplexer (ADM) to add/drop signals  
propagating from right to left.

In other words, the input port of the de-  
multiplexer (D) is connected to port (4), the output  
port of the multiplexer (M) to port (1), and 2x2  
optical switches (Sw) to the de-multiplexer's output  
ports and the multiplexer's input ports. Then one can  
drop or add the signals with specific wavelengths if  
the remaining two ports of the optical switch are  
20 connected to the receiver (RX) and the transmitter  
(TX), respectively. Unlike the case of Figure 4, the  
4-port wavelength router still suppressed the multiple  
reflected lights.

25 The signals propagating from left to right can

also be added/dropped in the same manners. In this case, we use a symmetrically modified router (4pr), in which the signal paths for the Group C propagating from left to right and for Group D propagating from right to left are interchanged.

If the two symmetric routers are connected together, both signals of Group C (traveling from left to right) and Group D (traveling from right to left) can be added/dropped at the same time.

As we have seen above, the wavelength selective router (4pr) according the present invention is useful in WDM bidirectional optical transmissions. It suppresses the multiple reflections, the limiting factor of the bidirectional transmission systems and networks, and effectively routes the counter-propagating signals. Therefore, the wavelength selective router (4pr) according the present invention simplifies the bidirectional signal transmissions with low cost.

While the foregoing invention has been described in terms of the embodiments discussed above, numerous variations are possible. Accordingly, modifications and changes such as those suggested above, but not